Gate-Bias Control Technique for Envelope Tracking Doherty Power Amplifier

Envelope Tracking 도허티 전력 증폭기의 Gate-Bias Control Technique

Junghwan Moon·Jangheon Kim·Ildu Kim·Jungjoon Kim·Bumman Kim 문정환·김장헌·김일두·김정준·김범만

Abstract

The gate-biases of the Doherty power amplifier are controlled to improve the linearity performance. The linearity improvement mechanism of the Doherty amplifier is the harmonic cancellation of the carrier and peaking amplifier at the output power combining point. However, it is difficult to cancel the harmonic power for the broader power range because the condition for cancelling is varied by power. For the linearity improvement, we have explored the linearity characteristic of the Doherty amplifier according to the input power and gate biases of the carrier and peaking amplifier. To extend the region of harmonic power cancellation, we have injected the proper gate bias to the carrier and peaking amplifier according to the input power levels. To validate the linearity improvement, the Doherty amplifier is designed using Eudyna 10-W PEP GaN HEMT EGN010MKs at 2.345 GHz and optimized to achieve a high linearity and efficiency at an average output power of 33 dBm, backed off about 10 dB from the P_{1dB}. In the experiments, the envelope tracking Doherty amplifier delivers a significantly improved adjacent channel leakage ratio performance of -37.4 dBc, which is an enhancement of about 2.8 dB, maintaining the high PAE of about 26 % for the WCDMA 1-FA signal at an average output power of 33 dBm. For the 802.16-2004 signal, the amplifier is also improved by about 2 dB, -35 dB.

요 약

본 논문에서는 선형성 증가를 위해 도허티 증폭기의 게이트 바이어스를 조정하는 방식을 제시하였다. 도허티 증폭기의 선형성 향상은 출력 결합 지점에서의 고조파 상쇄를 통해 이루어진다. 하지만 고조파의 상쇄는 그 크 기와 위상이 출력 지점에서 같은 크기와 서로 다른 위상을 가지고 있어야 이루어질 수 있는데, 넓은 출력 전력 범위에서 위와 같은 조건을 만족시키는 것은 쉽지 않다. 선형성 증가를 위해 도허티 증폭기의 캐리어 증폭기와 피킹 증폭기의 선형성 특성을 입력 전력과 각 증폭기의 게이트 바이어스를 조정함으로써 살펴보았다. 살펴본 특성을 기본으로 하여 고조파 상쇄 전력 범위를 증가시키기 위해, 각 전력 레벨에 맞는 게이트 바이어스를 증폭 기에 인가하였다. 게이트 바이어스 제어를 통한 선형성 향상을 알아보기 위해, 2.345 GHz에서 Eudyna사의 10-W PEP GaN HEMT EGN010MK 소자를 이용하여 도허티 전력 증폭기를 설계하였고, P_{1dB}로부터 10 dB back-off 지 점인 33 dBm에서 고효율과 고선형성을 위해 최적화 되었다. WCDMA 1-FA 신호에 대해 제안된 게이트 바이어 스 컨트롤 된 도허티 증폭기는 2.8 dB의 선형성 개선을 확인할 수 있었으며, 26 %의 PAE를 확인할 수 있었다.

^TThis work was supported in part by the Ministry of Knowledge Economy, Korea, under the Information Technology Research Center (ITRC) support program supervised by the Institute of Information Technology Advancement(IITA) (IITA-2008-C1090-0801-0037) and partially sponsored by ETRI SoC Industry Promotion Center, Human Resource Development Project for IT SOC Architect.

포항공과대학교 전자전기공학부(Dept. of Electronics and Electrical Engineering, Pohang University of Science and Technology(POSTECH)) · 논 문 번 호 : 20080523-01S

[·] 수정완료일자 : 2008년 7월 28일

또한, 802.16-2004 신호에 대해 RCE가 2 dB 증가됨을 확인할 수 있었다.

Key words : Doherty Amplifier, Envelope Tracking, Gate Bias Control, GaN HEMT Amplifier, Linearity Improvement Technique, WCDMA, WiMAX

I. Introduction

Current and next generation communication systems are required to transmit amount of data for various contents. As a result, the signals of the systems have large peak-to-average power ratios(PAPRs) caused by complex modulation scheme to efficiently use the frequency resource. To amplify these signals linearly, the power amplifier(PA) should be operated at a large backed-off output power region, which cause the degradation of efficiency performance. To improve the efficiency of the PA, many techniques are proposed recently, such as envelope tracking, envelope elimination and restoration, and so on. Among them, the Doherty PA is a good choice for the modern communication systems because of high efficiency performance at the large backed-off power levels with simple circuit topology and many researches are verified this. Moreover, a harmonic cancellation mechanism between the carrier and peaking amplifier of the Doherty topology using the derivative superposition method improved the linearity performan $ce^{[1]\sim[3]}$. However, it is difficult to satisfy the harmonic cancellation conditions over the broader power levels since the conditions are changed by various elements, such as input power level and gate bias of each amplifier^[4].

To extend the harmonic cancellation power ranges and improve the linearity performance of the Doherty PA, we have proposed the Doherty amplifier employing the gate-bias control technique according to the magnitude of the envelope signal, which is described in section II. To verify the linearity improvement through the extension of the harmonic cancellation power regions, we have simulated on the advanced design system (ADS) using Freescales 4-W PEP LDMOSFET MRF-281SR1s at the 2.14 GHz and experimented using Eudyna 10-W PEP GaN HEMT EGN010MKs at the 2.345 GHz. Based on a two-tone test, we have selected the proper gate biases of the carrier and peaking amplifiers according to the power level, and then we have injected the proper gate biases to the carrier and peaking amplifiers. For the WCDMA-1FA and IEEE 802.16-2004 signal test, the improved linearity performances of the envelope tracking Doherty amplifier employing gate bias control technique are demonstrated.

II. Gate Bias Control by Employing Envelope Tracking Technique

It is well known that the linearity improvement mechanism of the Doherty PA is cancellation of the thirdorder inter-modulation(IM3) between the carrier and peaking amplifiers. When the IM3 characteristics of the amplifiers are perfectly satisfied with the equations (1) and (2), the IM3 power is cancelled out maximally at the output combining point of the Doherty topology,

$$\left|IM \,\mathbf{3}_{C}\right| = \left|IM \,\mathbf{3}_{P}\right| \tag{1}$$

$$\angle IM \, \mathbf{3}_C = \angle IM \, \mathbf{3}_P \pm \pi \,. \tag{2}$$

However, the IM3 magnitude and phase of each amplifier are functions of the gate bias, power level, and so on, so it is very difficult to satisfy the conditions of equations (1) and (2) for the wide power ranges. To extend the IM3 cancellation power regions of the Doherty amplifier, we have selected the proper gate biases for each input power level. Figs. 1(a) and (b) show the measured inter-modulation distortion(IMD) characteristics with and without gate bias adaptation according to the power levels and selected gate biases of each amplifier for the two-tone signal with 1 MHz tone spacing. The gate biases are selected for optimizing the IMD3 characteristic at each power level and controllable sha-



Fig. 1. (a) Measured IMD characteristics with and without gate bias control. (b) Gate biases of the carrier and peaking amplifiers for optimizing the IMD3 characteristic.

pes. By adjusting the gate biases, we could obtain more linear characteristic over the broader power levels.

III. Simulation and Experimental Results

3-1 Simulation Results

For verifying the linearity improvement using the gate-bias envelope tracking, we have simulated on ADS 2004A. The simulated Doherty amplifier is designed using two cells of Freescales 4-W peak envelope power LDMOSFET MRF281SR1s. The amplifier handles about 40 dBm of P_{1dB} at 2.14 GHz and was optimized to achieve high linearity and efficiency at an average output power of 30 dBm.

Figs. 2(a) and (b) show the simulated IMD characteristics of the class-AB and Doherty PA with and without gate bias adaptation, and gate biases of the carrier and peaking amplifiers. From the Fig. 2(a), we can recognize more linear characteristic of the gate-bias adapted Doherty amplifier than others. Fig. 2(c) shows the simulated adjacent channel leakage ratio(ACLR) performance of the class-AB and Doherty amplifiers with and without gate bias control for the CDMA signal with PAPR of about 10 dB. As expected, ACLR performance of the proposed Doherty amplifier is enhanced over the border output power ranges, thanks to the extension of the IM3 cancellation power regions.

3-2 Experimental Results

To validate the linearity improvement employing the gate-bias envelope tracking, we have designed the Doherty amplifier using Eudyna 10-W peak envelope power GaN HEMT EGN010MKs. The amplifier can handle a 43 dBm of P_{1dB} at 2.345 GHz. In the experiments, the quiescent biases and individual matching circuitry of the carrier and peaking amplifiers are selected to maximally cancel the ACLR performance at an average output power of 33 dBm, backed-off about 10 dB from the P_{1dB} .

Fig. 3 shows the experimental setup for gate-bias envelope tracking experiment, which consists of ADS as an I and Q data source for WCDMA 1-FA signal and IEEE 802.16-2004 fixed WiMAX signal, MATLAB as a digital signal processor(DSP) for shaping the gate biases of the carrier and peaking amplifiers, ESG E4438C as a modulator for WCDMA 1-FA and IEEE 802.16-2004 signal sources, and PSG E8267D as a digital to analog converter(DAC) for the shaped gate bias sources. The output signal of DAC is amplified or shifted by differential OP-AMP voltage amplifiers. Then, the gate bias signals are injected to the each amplifier. Initial gate biases are shaped by the measured two-tone test depicted in the Fig. 1(b), and we have optimized the gate biases of the carrier and peaking amplifier in the



Fig. 2. (a) Simulated IMD characteristics with and without gate bias control. (b) Gate biases of the carrier and peaking amplifiers for optimizing the IMD3 characteristic. (c) Simulated ACLR performance of class-AB and Doherty amplifiers with and without gate bias control.



Fig. 3. Test bench for gate-bias envelope tracking.

experiment. Moreover, delay between gate bias and RF source path is adjusted by changing the length of cables and by altering the number of delay tap on the ADS simulator.

Fig. 4 shows the gate biases of the carrier and peaking amplifiers, which are shaped from the Fig. 1(b) and modified to maximize the linearity improvement, and WCDMA 1-FA envelope signal at the average output power of 33 dBm. From this figure, we can confirm delay between gate bias and RF source path don't exist. Fig. 5 shows the measured output spectra of the fixed and adapted gate bias for the Doherty PA at an average output power of 33 dBm. From the output spectra, we can recognize more linear characteristic of the proposed Doherty amplifier. Table 1 shows the summary of the measured performance for WCDMA 1-FA signal. Although the gate bias envelope tracking technique is in-



Fig. 4. Measured gate biases of the carrier and peaking amplifiers and envelope signal for WCD-MA 1-FA signal.



Fig. 5. Measured output spectra of the fixed and adapted gate bias for Doherty amplifier at average output power of 33 dBm.

Table	1.	Summary of the measured performance at an
		average output power of 33 dBm for WCD-
		MA 1-FA signal.

	Gain [dB]	PAE [%]	ACLR [dBc] +2.5/-2.5 MHz
Doherty (Fixed Bias)	14.3	25.6	-34.8/-35.0
Doherty (Bias Adaptation)	14.1	26.1	-37.4/-38.9

tended to enlarge the IM3 cancellation power range for linearity improvement, the PAE is also enhanced slightly due to the lower gate biases for the carrier and peaking amplifiers compared to the fixed gate bias Doherty amplifier.

Fig. 6 shows the gate biases of the carrier and peaking amplifiers and IEEE 802.16-2004 envelope signal at the average output power of 33 dBm. Figs. 7 show the measured signal constellation diagrams of the fixed and adapted gate bias for the Doherty amplifier at the average output power of 33 dBm. In comparison with the signal constellation diagram of the conventional Doherty amplifier, we can recognize the diagram of the gate bias controlled Doherty amplifier is clearer, which means the proposed Doherty amplifier can amplify the signal more linearly. Table 2 shows the summary of the measured performance for IEEE 802.16-2004 signal.



Fig. 6. Measured gate biases of the carrier and peaking amplifiers and envelope signal for IEEE 802.16-2004 signal.



Fig. 7. Measured signal constellation diagram of (a) fixed gate bias and (b) controlled gate bias for the Doherty amplifier at the average output power of 33 dBm.

Table 2.	Summary of the measured performance at an
	average output power of 33 dBm for IEEE
	802.16-2004 signal.

	Gain [dB]	PAE [%]	RCE [dB]
Doherty (Fixed Bias)	14.3	25.6	-33
Doherty (Bias Adaptation)	14.1	25.4	-35

IV. Conclusion

We have implemented the gate-bias envelope tracking Doherty amplifier to improve the linearity performance. To extend the IM3 cancellation power regions, the proper gate biases are chosen through the twotone test. Based on the measured gate biases according to the power levels, the dynamic gate bias adjustment of the carrier and peaking amplifiers is employed to maximize the harmonic cancellation. In the experiments, the gate-bias adapted Doherty amplifier delivers a lot more linear characteristic than the fixed gate-bias Doherty amplifier.

References

- S. C. Cripps, *RF Power Amplifiers for Wireless Communications*, Norwood, MA: Artech House, 2002.
- [2] Y. Yang, J. Yi, Y. Y. Woo, and B. Kim, "Optimum design for linearity and efficiency of microwave Doherty amplifier using a new load matching technique", *Microw. J.*, vol. 44, no. 12, pp. 20-36, Dec. 2001.
- [3] F. H. Raab, P. Asbeck, S. Cripps, P. B. Kenington, Z. B. Popovic, N. Pothecary, J. F. Sevic, and N. O. Sokal, "Power amplifier and transmitters for RF and microwave", *IEEE Trans. Microw.*, *Theory Tech.*, vol. 50, no. 3, pp. 814-826, Mar. 2002.
- [4] J. Moon, J. Kim, I. Kim, J. Kim, and B. Kim, "A wideband envelope tracking Doherty amplifier for WiMAX systems", *IEEE Microw. and Wireless Compon. Lett.*, vol. 18, no. 1, pp. 49-51. Jan. 2008.

문 정 환



2006년 2월: 서울시립대학교 전자 컴퓨터공학부 전자공학과 (공학 사)

2006년 3월~현재: 포항공과대학교 전자컴퓨터공학부 전자과 박사과 정

[주 관심분야] 고효율 고선형성 RF

전력 증폭기 설계 및 메모리 영향 보상 기술 연구, 디지 털 전치 왜곡 선형화 기술 연구

김 장 헌



2003년 2월: 전북대학교 전자정보 공학부 전자공학과 (공학사) 2003년 3월~현재: 포항공과대학교 전자컴퓨터공학부 전자과 박사과 정

[주 관심분야] 고효율 고선형성 RF 전력 증폭기 설계 및 메모리 영

향 보상 기술 연구, 디지털 전치 왜곡 선형화 기술 연구

김 일 두



2004년 2월: 전남대학교 정보통신 공학부 전자공학과 (공학사) 2004년 3월~현재: 포항공과대학교 전자컴퓨터공학부 전자과 박사과 정

[주 관심분야] RF 전력 증폭기 설계 및 선형전력 증폭기(LPA) 시스템

설계, 기지국용 고효율 전력 송신기 설계

김 정 준



2007년 2월: 한양대학교 전자공학 부 전자공학과 (공학사)

2007년 3월~현재: 포항공과대학교 전자컴퓨터공학부 전자과 석사과 것

[주 관심분야] 고효율 고선형성 RF 전력 증폭기 설계 김 범 만



1979년 2월: 카네기 멜론대학 전자 공학과 (공학박사)

1978년~1981년: GTE Lab. 연구원 1981년~1988년: TI Central Research Lab. 연구원

1989년~2003년: 포항공과대학교 전 자컴퓨터공학부 정교수

1994년~2004년: 포항공과대학교 마이크로웨이브 응용 연 구센터(MARC, funded by ADD) 센터장

2002년 7월~2005년 6월: T-MTT Associate Editor(IEEE)

2003년 4월~현재: 포항공과대학교 전자컴퓨터공학부 BK 사업 단장

2003년~2004년: 한국과학기술한림원 종신회원 및 공학 부정보통신 분과장

2004년~2005년: 대한전자공학회 협동 부회장

2004년~현재: 포항공과대학교 전자컴퓨터공학부 남고석 좌교수

2005년 1월~2007년 12월: Distinguished Lecturer(IEEE MTT society)

2006년~현재: 포항공과대학교 전자컴퓨터공학부 주임교 수

2007년 1월~현재: IEEE Fellow 선정

[주 관심분야] 이동통신용 전력 증폭기, RF 회로 설계 및 소자 모델링, III-V 화합물 반도체, 초고주파 집적회로 (MMIC) 설계 및 구현, 밀리미터 웨이브 회로 설계